

**The W-WO<sub>2</sub> oxygen fugacity buffer (WWO) at high pressure and temperature:  
Implications for fO<sub>2</sub> buffering and metal-silicate partitioning.**

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**Abstract**

Synchrotron x-ray diffraction data were obtained to simultaneously measure unit cell volumes of W and WO<sub>2</sub> at pressures and temperatures up to 70 GPa and 2300 K. Both W and WO<sub>2</sub> unit-cell volume data were fit to Mie-Grüneisen equations of state; parameters for W are  $K_T = 307 (\pm 0.4)$  GPa,  $K_T' = 4.05 (\pm 0.04)$ ,  $\gamma_0 = 1.61 (\pm 0.03)$ , and  $q = 1.54 (\pm 0.13)$ . Three phases were observed in WO<sub>2</sub> with structures in the P2<sub>1</sub>/c, Pnma and C2/c space groups. The transition pressures are 4 GPa and 32 GPa for the P2<sub>1</sub>/c-Pnma and Pnma-C2/c phase changes, respectively. The P2<sub>1</sub>/c and Pnma phases have previously been described whereas the C2/c phase is newly described here. Equations of state were fitted for these phases over their respective pressure ranges yielding the parameters  $K_T = 238 (\pm 7)$ , 230 ( $\pm 5$ ), 304 ( $\pm 3$ ) GPa,  $K_T' = 4$  (fixed), 4 (fixed), 4 (fixed) GPa,  $\gamma_0 = 1.45 (\pm 0.18)$ , 1.22 ( $\pm 0.07$ ),

32 1.21 ( $\pm 0.12$ ), and  $q = 1$  (fixed), 2.90 ( $\pm 1.5$ ), 1 (fixed) for the P2<sub>1</sub>/c, Pnma and C2/c phases,  
33 respectively. The W-WO<sub>2</sub> buffer (WWO) was extended to high pressure using these W and  
34 WO<sub>2</sub> equations of state. The T-fO<sub>2</sub> slope of the WWO buffer along isobars is positive from  
35 1000 to 2500K with increasing pressure up to at least 60 GPa. The WWO buffer is at a  
36 higher fO<sub>2</sub> than the iron-wüstite (IW) buffer at pressures lower than 40 GPa, and the  
37 magnitude of this difference decreases at higher pressures. This implies an increasingly  
38 lithophile character for W at higher pressures. The WWO buffer was quantitatively applied  
39 to W metal-silicate partitioning by using the WWO-IW buffer difference in combination  
40 with literature data on W metal-silicate partitioning to model the exchange coefficient ( $K_D$ )  
41 for the Fe-W exchange reaction. This approach captures the non-linear pressure dependence  
42 of W metal-silicate partitioning using the WWO-IW buffer difference. Calculation of  $K_D$   
43 along a peridotite liquidus predicts a decrease in W siderophility at higher pressures that  
44 supports the qualitative behavior predicted by the WWO-IW buffer difference, and agrees  
45 with findings of others. Comparing the competing effects of temperature and pressure the  
46 results here indicate that pressure exerts a greater effect on W metal-silicate partitioning.

47 Keyword: high pressure, tungsten, oxygen fugacity buffer, equation of state, metal-silicate  
48 partitioning

49

## Introduction

50 Knowledge of volumetric properties of metals and oxides at high pressure and temperature  
51 contributes to our understanding of metal-silicate equilibria within planetary interiors, the latter  
52 of which can exert a strong influence on the chemical potential of oxygen (or oxygen fugacity,  
53 fO<sub>2</sub>). The coexistence of a metal and its oxide at equilibrium constitutes an oxygen buffer, and  
54 can be used in 1-bar or high pressure experimentation to control or calculate fO<sub>2</sub> (e.g., Cottrell et

55 al. 2009, 2010; Burkemper et al. 2012; Dobson and Brodholt, 1999; Rubie, 1999). A common  
56 example relevant to the deep Earth is the iron-wüstite (IW) buffer which is often used to control  
57 and measure the  $fO_2$  of Fe-bearing experiments. However, in non Fe-bearing experiments where  
58  $fO_2$  similar to IW is desired or in cases requiring  $fO_2$  conditions more oxidizing or reducing than  
59 IW, an alternative buffer must be used. The  $fO_2$  of the W-WO<sub>2</sub> (WWO) buffer is equal to IW at  
60 approximately 1200 K (at 1 bar), and becomes more oxidizing with increasing temperature,  
61 becoming approximately one log unit higher at 2200 K. For this reason, the WWO buffer is well-  
62 suited to experiments where  $fO_2$  similar to that of IW is required, e.g. Cottrell et al. (2009, 2010)  
63 controlled and calculated experimental  $fO_2$  using the WWO buffer in Fe-free, W-bearing melting  
64 experiments.

65 Oxygen fugacity buffers can have significant pressure dependencies. The volume  
66 difference between the metal and oxide of a buffer is used to obtain  $fO_2$  along the buffer at high  
67 pressures, and therefore differences in compressibility of the metal and oxide can result in  
68 significant deviations of calculated  $fO_2$  relative to 1-bar. The WWO buffer has been studied at  
69 ambient pressure conditions and at temperatures up to approximately 1700K (O'Neill and  
70 Pownceby 1993), but it has no experimental constraints at high pressure. Extension of the 1-bar  
71 buffers for application to high pressure experiments or to the conditions of the deep Earth  
72 requires precisely determined phase volumes of the metal and oxide phases at high pressure  
73 (Campbell et al. 2009), which can be calculated using equations of state.

74 The equation of state of W has been determined using extensive high pressure and  
75 temperature experimental constraints (Houska, 1964; Grimvall et al., 1987; Dewaele et al. 2004;  
76 Dorogokupets and Oganov 2007). The equation of state of WO<sub>2</sub>, however, is limited to room-  
77 temperature elastic parameters determined from a computational study with no experimental

78 constraints (Dewhurst and Lowther 2001). Known phases of  $\text{WO}_2$  are a  $P2_1/c$  structure at 1-bar  
79 (Bolzan et al. 1995) and a  $Pnma$  structure that was synthesized at 8 GPa and 1120 K and  
80 characterized by x-ray diffraction at 1-bar and room temperature (Sundberg et al. 1994). The  
81  $P2_1/c$  and  $Pnma$  structured phases will be referred to as  $ap\text{-WO}_2$  and  $hp\text{-WO}_2$  following the  
82 naming convention of Sundberg et al. (1994). Nothing is known experimentally about  $\text{WO}_2$  at  
83 pressures and temperatures higher than the studied conditions of the  $hp\text{-WO}_2$  phase, and  
84 consequently the behavior of the WWO buffer is imprecisely constrained at higher pressures.  
85 Therefore, we have conducted high pressure and high temperature experiments to characterize  
86 the WWO buffer. The data are also applied to better understand the thermodynamics of W  
87 partitioning between metal and silicate under magma ocean conditions. The experimental work  
88 to characterize the WWO buffer was conducted using both diamond anvil cell (DAC) and multi-  
89 anvil press (MAP) techniques in conjunction with synchrotron x-ray diffraction.

### 90 **Synchrotron X-ray diffraction experiments**

91 To obtain thermal equations of state (EOS) and oxygen fugacity buffers for the W- $\text{WO}_2$   
92 system, x-ray diffraction data were collected on coexisting W and  $\text{WO}_2$ . The sample materials  
93 were mixtures of approximately 1:1 by weight of W: $\text{WO}_2$  using powders acquired from Alfa-  
94 Aesar (>99.9% pure). Room-temperature DAC compression experiments included Pt as a  
95 pressure standard and the mixture was approximately 1:1:1 by weight of W: $\text{WO}_2$ :Pt. Powders  
96 were ground under ethanol in agate mortars to ~1 micron grain size for DAC experiments; for  
97 MAP experiments the powder mixtures were ground for approximately 15 minutes to  
98 homogenize the distribution of the phases. These data were collected across a wide range of  
99 pressures and temperatures (Figure 1) using diamond anvil cells at beamline X17C of the  
100 National Synchrotron Light Source (NSLS), Brookhaven National Laboratory, and using

101 diamond anvil cells and a multi anvil press at beamline 13-ID-D of the Advanced Photon Source  
102 (APS), Argonne National Laboratory. Making measurements of both metal and oxide in the  
103 same experiment was important because the oxygen fugacity buffer is defined in terms of the  
104 equilibrium between metal and oxide. It was also advantageous that both phases are present  
105 under the same experimental conditions in EOS calculations because the volume differences  
106 ( $\Delta V$ ) between the phases were referenced to exactly the same P-T conditions. This reduced or  
107 eliminated uncertainties due to pressure standardization and heterogeneous experimental  
108 conditions (P or T gradients) when coupling the two EOS for consideration of the metal-oxide  
109 buffer.

#### 110 **Diamond anvil cell**

111 Room temperature compression provides the foundation for the thermal EOS. Coexisting W  
112 and  $WO_2$  were compressed in DACs using an argon pressure medium over a pressure range of  
113 approximately 25 to 73 GPa. X-ray diffraction data were collected on beamline X17C at NSLS  
114 using angle-dispersive diffraction with diffraction patterns collected on a CCD (MAR) x-ray area  
115 detector. These x-ray diffraction data were used to determine unit cell volumes of the individual  
116 phases. Experimental pressures were determined using Pt as a pressure standard (Fei et al. 2007).  
117 The W data were included in the calculation of the W EOS as discussed in later sections. The  
118 room temperature  $WO_2$  data were not included in EOS calculations because robust unit-cell  
119 volumes could not be obtained due to a sluggish phase transition from the *ap*- $WO_2$  to the *hp*-  
120  $WO_2$  phase at room temperature. As discussed in later sections, the *ap*- $WO_2$  and the *hp*- $WO_2$   
121 phases coexisted over a pressure range of at least 20 GPa, which was evidenced by peaks for  
122 both phases in diffraction patterns over this pressure range.

123 Laser-heated DAC experiments were conducted at APS on coexisting W and  $WO_2$  where x-

124 ray diffraction data were collected at temperatures up to approximately 2250 K and at pressures  
125 up to approximately 70 GPa. The sample was prepared by compression of the starting mixture  
126 into a thin layer that was  $\sim 5 \mu\text{m}$  thick. The sample was loaded into a symmetric-type DAC  
127 between layers of NaCl that served as both insulator and as a pressure standard (Decker 1971;  
128 Fei et al. 2007). The Pt pressure scale used in the 300 K experiments was calibrated with the  
129 NaCl pressure scale used in the high temperature experiments – both used Fei et al. (2007). The  
130 sample chamber was made by drilling an 80 micron hole in a pre-indented rhenium gasket and  
131 was compressed between diamond anvils with 250 micron culet diameters. The monochromatic  
132 x-ray source had a wavelength of  $0.3344 \text{ \AA}$  and was focused to a spot size of  $\sim 3 \mu\text{m}$  diameter.  
133 The diffraction data were measured using an angle-dispersive configuration and diffraction  
134 patterns were collected using a MAR165 CCD x-ray area detector with the sample to detector  
135 distance calibrated by 1-bar  $\text{CeO}_2$  diffraction patterns. The sample was heated on both sides  
136 using twin ytterbium fiber lasers with approximate spot sizes of 20 microns (Prakapenka et al.,  
137 2008). Laser powers were adjusted to equalize the temperatures on the two sample surfaces. The  
138 lasers were directed onto the sample using x-ray transparent optics which permitted the laser and  
139 x-ray beams to be coaxial, and allowed for collection of x-ray diffraction data at high  
140 temperatures (Shen et al. 2001). Temperatures were measured using spectro-radiometry and the  
141 resulting thermal emission spectra were fitted to the Planck function using the greybody  
142 approximation (Heinz and Jeanloz 1987). These measurements were of the temperature at the  
143 interface between the sample and the insulating layer, i.e. at the surface of the sample, and over  
144 an area of approximately  $5 \times 5$  microns at the center of the laser-heated spot. The sample in this  
145 experiment was opaque and most of the laser radiation was absorbed at the sample surface, and  
146 consequently the temperature in the axial center of the sample where it was being probed by the

147 x-ray beam was slightly lower than the measured temperature. The reported experimental  
148 temperatures were corrected for this axial thermal gradient, which was an approximately three  
149 percent decrease from the measured temperatures, based on an approximate sample thickness of  
150 5 microns (Campbell et al. 2007; 2009). Because of technical difficulties with the downstream  
151 (relative to the x-ray beam) temperature measurements during these experiments, the  
152 temperatures reported here are those measured in the upstream direction only (Fischer et al.,  
153 2011). Four heating cycles were made, with starting pressures of approximately 18, 39, 53, and  
154 67 GPa at ambient temperature; these are hereafter referred to as the 20, 40, 55, and 70 GPa  
155 cycles. Laser power was gradually increased and diffraction patterns were collected up to the  
156 peak temperature for a given pressure step. The laser power was then decreased gradually and  
157 diffraction patterns were collected approximately every 100 degrees. The pressure in the  
158 diamond cell was increased at room temperature between each heating cycle. The diffraction  
159 data from the cooling portion of each heating cycle were used in EOS calculations to minimize  
160 uncertainties related to non-hydrostatic stresses, which are greatly reduced after high temperature  
161 treatment.

162 Resistively-heated DAC experiments (RHDAC) were made using an external heating system  
163 that was developed in the University of Maryland Laboratory for Mineral Physics, which  
164 allowed for sample chamber temperatures up to approximately 725 K. This heater design  
165 completely enclosed a Tel-Aviv-type DAC, which minimized temperature gradients but caused  
166 the pressure to decrease during heating. X-ray diffraction data were collected at beamline X17C  
167 at NSLS using this DAC assembly. Diffraction patterns were collected at discrete temperatures  
168 and at four different starting pressures. The sample was insulated between layers of NaCl, which  
169 also served as a pressure calibrant (Decker 1971; Fei et al. 2007). Temperatures were measured

170 using a type K thermocouple that was placed at the contact between the diamond culets. This  
171 was done by wrapping the thermocouple loop around the diamonds and cementing the loop to  
172 the gasket using alumina cement obtained from Zircar Ceramics.

### 173 **Multi anvil press**

174 Diffraction patterns were collected using the T25 module in the 1000 ton MAP using a  
175 COMPRES octahedral 10/5 assembly (Leinenweber et al. 2006), at beamline 13-ID-D at the  
176 Advanced Photon Source. Boron nitride capsules were used because their low mean atomic  
177 number results in minimal attenuation of the x-ray beam, and samples were heated with Re or  
178  $\text{LaCrO}_3$  (Leinenweber et al., 2006, 2012) heaters. The entire cube assembly was aligned to allow  
179 the x-ray beam to pass between the gaps of the WC cubes, the “equatorial“ graphite window, and  
180 slits in the Re and  $\text{LaCrO}_3$  in the octahedral assembly. Diffracted x-rays were detected using a  
181 cooled Ge energy-dispersive detector placed at a fixed  $2\theta$  angle of  $6^\circ$  relative to the incoming x-  
182 ray beam.

183 The sample capsule had two chambers; one contained a mixture of W and  $\text{WO}_2$ , and the  
184 other contained MgO as a pressure calibrant. The equation of state for MgO of Speziale et al.  
185 (2001) was used and is compatible with the Pt and NaCl EOS of Fei et al. (2007) described  
186 above. An initial heating cycle was made at a press force of 800 tons corresponding to a pressure  
187 of approximately 20 GPa at 2100 K. Similar to LHDAC experiments, data were collected on the  
188 heating and cooling portions of this cycle but only the cooling data were used in EOS  
189 calculations. It was noted during the second cycle, at 400 tons press force, that the W diffraction  
190 peaks were weakening in relative intensity to those of  $\text{WO}_2$ . At this point the experiment was  
191 decompressed at constant temperature; data obtained at press forces of 350 and 270 tons were  
192 used in EOS calculations. Examination of the run product from this experiment revealed no W



193 metal, which suggests that the metal became oxidized over the course of the experiment which is  
194 why the W diffraction intensities decreased so significantly. Tungsten carbide was not observed  
195 either. The WO<sub>2</sub> remained a stable phase, consistent with successful indexing of the diffraction  
196 data to the published orthorhombic (Pnma) structure (Sundberg et al. 1994). Microprobe  
197 analyses of the WO<sub>2</sub> yielded W contents consistent with a stoichiometric phase, but future work  
198 may want to examine this in more detail and for all three WO<sub>2</sub> phases.

### 199 **Data Analysis**

200 The foundational data for characterizing the equations of state were x-ray diffraction patterns  
201 in the form of either two-dimensional CCD images or one-dimensional energy spectra collected  
202 by a solid-state Ge, energy-dispersive detector. The 2-d diffraction patterns were calibrated with  
203 CeO<sub>2</sub> and processed using the Fit2D software, which integrates a diffraction image to produce a  
204 1-d spectrum of 2θ angle versus intensity (Hammersley et al., 1996). The 1-d energy dispersive  
205 spectra were converted to *d*-spacing versus intensity spectra by applying energy and 2θ  
206 calibrations. Energy calibrations were based on radioactive <sup>57</sup>Co and <sup>109</sup>Cd sources, and Ag K<sub>α</sub>  
207 and K<sub>β1</sub> lines. The 2θ calibration was based on a 1-bar x-ray diffraction pattern of Al<sub>2</sub>O<sub>3</sub>. The x-  
208 ray diffraction peaks in the experimental spectra were fitted using the PeakFit™ software by  
209 SeaSolve Software Inc., which also allowed for background subtraction.

210 Because the difference in molar volume between the phases is used to calculate the fO<sub>2</sub> of the  
211 WWO buffer, the principal information needed was the molar volumes of the W and WO<sub>2</sub> phases  
212 at each P-T point. The molar volumes were calculated using the unit cell volumes and the  
213 number of formula units per unit cell (*Z*).

214 Tungsten, sodium chloride, magnesium oxide, and platinum are cubic and for each reflection  
215 a lattice parameter *a* was calculated from the measured *d*-spacings and the assigned Miller

216 indices  $h k l$  by the equation,  $a = d_{meas}\sqrt{h^2 + k^2 + l^2}$ . The average of these calculated lattice  
217 parameters was taken as the lattice parameter for each phase in each pattern, and uncertainties  
218 were calculated as the standard error of the mean. See Supplementary Data for lattice parameters,  
219 and experimental pressures and temperatures (Table S1).

220 The pressure was calculated based on the equation of state of W (Dorogokupets and Oganov,  
221 2007). Although other materials with well calibrated equations of state were included in each  
222 experiment (MgO in the MAP experiments; NaCl as the insulator / pressure medium in  
223 LHDAC/RHDAC experiments; Pt in room temperature DAC experiments), we found that the  
224 most reproducible results were obtained using W as the pressure standard, because it was  
225 intimately mixed with the  $WO_2$  sample and at identical P–T conditions, whereas the same may  
226 not have been the case for MgO and NaCl. The primary difference in experimental conditions  
227 between W and either MgO or NaCl was likely temperature, i.e. slightly different physical  
228 location in the presence of a thermal gradient resulted in differences in thermal pressures in the  
229 phases. Consideration of the experimental configurations in comparison to the differences in  
230 pressures calculated using W and either MgO or NaCl supports this interpretation. For example  
231 in the MAP experiments the MgO was separate from but adjacent to the sample chamber, and the  
232 W and MgO pressures were largely consistent within uncertainties (~1 GPa). The temperature  
233 difference across this distance could have been up to approximately 100 K (Leinenweber et al.  
234 2012), which would contribute to an approximately 0.5 GPa difference in calculated pressure of  
235 either W or MgO. The NaCl thermal gradient in the RHDAC experiments, in which the entire  
236 cell was heated, was likely less than 100 K, and the W and NaCl pressures were likewise  
237 consistent within uncertainties. In contrast, the axial thermal gradient through the NaCl layers in  
238 the LHDAC experiments was large with a correspondingly higher level of uncertainty on the

239 range of temperatures of the NaCl probed by the x-ray beam. In the room-temperature DAC  
240 experiments, some of the pressures calculated using Pt and W differed outside of uncertainties,  
241 probably because of nonhydrostatic stresses at low temperature.

## 242 **Tungsten dioxide phases**

243 Both monoclinic and orthorhombic WO<sub>2</sub> phases (*ap*-WO<sub>2</sub> and *hp*-WO<sub>2</sub>) have been described  
244 in the literature (Bolzan et al. 1995, Sundberg et al. 1994). In the present experiments, both of  
245 these phases were observed in addition to a previously unpublished higher pressure and  
246 temperature monoclinic phase (*hpm*-WO<sub>2</sub> as described below). Miller indices were assigned to  
247 each identified peak in the patterns and lattice parameters were calculated using nonlinear least-  
248 squares minimization of the differences ( $\Delta d$ ) of measured and calculated *d*-spacings.

249 In the crystal structures of both the *ap*-WO<sub>2</sub> and *hp*-WO<sub>2</sub> phases, the W atoms occupy one  
250 half of the octahedral sites. The *ap*-WO<sub>2</sub> structure is characterized by chains of W octahedra in a  
251 distorted rutile type structure. The *hp*-WO<sub>2</sub> structure is characterized as a twinned 1-bar structure  
252 (Sundberg et al. 1994). The W-W distances in the *hp*-WO<sub>2</sub> structure are shorter than in the *ap*-  
253 WO<sub>2</sub> structure by 0.5 to 0.7 Å. This contributes to the higher density of *hp*-WO<sub>2</sub> and therefore its  
254 thermodynamic stability at higher pressure.

255 The higher pressure monoclinic WO<sub>2</sub> phase (*hpm*-WO<sub>2</sub>) was discovered during peak  
256 indexing of the LHDAC data. Comparison of peaks in the 20 GPa heating cycle were made to  
257 the 40 GPa heating cycle and it was apparent that the *Pnma*-structured *hp*-WO<sub>2</sub> phase was not  
258 present (Sundberg et al. 1994). The major orthorhombic peaks, (*111*) and (*230*) that were present  
259 in all 20 GPa patterns were absent in the 40 GPa and higher pressure data (Figure 2). Some  
260 similarities were observed between the 40, 55 and 70 GPa cycles, though additional peaks were  
261 present in the 55 and 70 GPa data suggesting that an additional phase was present at pressures

262 greater than 55 GPa. The diffraction pattern from this high pressure  $\text{WO}_2$  phase was indexed  
263 using the method of successive dichotomy as coded in the DICVOL powder indexing software of  
264 Boultif and Louer (2004).

265 To assess the robustness of this method, DICVOL pattern indexing was conducted using the  
266 patterns from each of the temperatures in the 20 GPa cooling cycle. All solutions were in the  
267 orthorhombic crystal system, and ultimately solutions were obtained for multiple diffraction  
268 patterns that were in agreement with the *Pnma* structure of Sundberg et al. (1994). The  
269 diffraction spectrum for G33\_006 (highest temperature pattern) compared to the 1-bar spectrum  
270 calculated using the Sundberg et al. (1994) structure data are shown in Figure 3. See  
271 Supplementary Data for lattice parameters, and experimental pressure and temperature  
272 conditions (Tables S2, S3 and S4).

273 Patterns from the 40 GPa data were likewise analyzed using DICVOL and all solutions were  
274 in the monoclinic system. The best solution was indexed with all  $\Delta d$  values less than 0.004 Å.  
275 This structure was in the *P2/m* space group and is here termed *hpm-WO<sub>2</sub>* (for high pressure  
276 monoclinic) following the convention of Sundberg et al. (1994). The *P2/m* space group of the  
277 *hpm-WO<sub>2</sub>* phase was the reduced cell form. A preferred space group *C2/c* was determined using  
278 the chekcell software (Laugier and Bochu).

279 Solutions determined using DICVOL for all W-oxide peaks in the 55 and 70 GPa data sets  
280 were not equivalent with the *hpm-WO<sub>2</sub>* of the 40 GPa set. This was likely due to a mixing of  
281 peaks from multiple phases. Peak indexing of the *hpm-WO<sub>2</sub>* phase was based on 16 to 19 peaks  
282 in the 55 GPa data and 7 to 12 peaks in the 70 GPa data. The uncertainties on the lattice  
283 parameters for the 70 GPa data were approximately twice that of the lattice parameters for the 55  
284 GPa data because of larger  $\Delta d$  values and also fewer indexed peaks in the 70 GPa data. The

285 changes in density between the 40 and 55 GPa, and 55 and 70 GPa sets were approximately 3  
286 and 4 percent, respectively, calculated along isotherms at 1000, 1300, 1700, and 2000 K.

287 Attempts were made to index the higher pressure (>40 GPa) data to a monoclinic  $\text{WO}_3$   
288 structure (Bouvier et al. 2002), under the hypothesis that  $\text{WO}_2$  may have disassociated to  $\text{WO}_3$   
289 and metallic W. However, many prominent peaks could not be indexed and the calculated molar  
290 volumes were not reasonable in comparison to the results of Bouvier et al. (2002). The proposed  
291 orthorhombic unit cell of Dewhurst and Lowther (2001) also does not fit the high-P-T data  
292 collected on  $\text{WO}_2$ .

293 Under room temperature compression and at approximately 25 GPa, a structural  
294 transformation from monoclinic (*ap*- $\text{WO}_2$ ) to the orthorhombic structure of  $\text{WO}_2$  was evident.  
295 These two structures coexisted for at least 20 GPa, with the monoclinic phase (*ap*- $\text{WO}_2$ ) mostly  
296 disappearing above approximately 45 GPa. Indexing the room temperature x-ray diffraction data  
297 on the orthorhombic phase was not robust when referenced to either the Sundberg et al. (1994) or  
298 Dewhurst and Lowther (2001) high pressure structures. Probable explanations include an  
299 incomplete phase transition with a mixture of structural states, and structural distortions due to  
300 accumulated strain related to room temperature compression.

301 High pressure x-ray diffraction experiments in a resistively-heated DAC conducted up to  
302 approximately 42 GPa and at temperatures up to approximately 725 K also showed the  
303 coexistence of the monoclinic (*ap*- $\text{WO}_2$ ) and orthorhombic (*hp*- $\text{WO}_2$ ) structured phases above 30  
304 GPa. In the highest pressure, high-temperature data, the monoclinic and orthorhombic phases  
305 appeared to have roughly equal contributions to the x-ray diffraction patterns as gauged by  
306 relative peak intensities.

307 At higher temperatures the monoclinic (*ap*- $\text{WO}_2$ )-to-orthorhombic (*hp*- $\text{WO}_2$ ) transition was

308 much faster. In our multi anvil press experiments and the lowest-pressure LHDAC experiments  
309 (<25 GPa), *hp*-WO<sub>2</sub> was easily identified. One or two diffraction peaks in the patterns from these  
310 experiments could possibly have been attributed to the *ap*-WO<sub>2</sub> phase, but the relative intensities  
311 of these peaks were extremely low. The *hp*-WO<sub>2</sub> phase was observed at a pressure of  
312 approximately 5 GPa and 300 K in the MAP experiments following a high temperature cycle.  
313 This suggests that the *ap*-WO<sub>2</sub> to *hp*-WO<sub>2</sub> transition has a kinetic barrier at 300 K, but *hp*-WO<sub>2</sub> is  
314 stable to low pressure and temperature conditions. This is also supported by the fact that  
315 Sundberg et al. (1994) recovered their *hp*-WO<sub>2</sub> phase to ambient conditions for x-ray diffraction  
316 analysis and crystal structure refinement. We place the phase boundary for the *ap*-WO<sub>2</sub> to *hp*-  
317 WO<sub>2</sub> transition at 4 GPa (near 400 K).

318 In the 40 GPa data from the LHDAC experiments, the *hpm*-WO<sub>2</sub> phase replaced the *hp*-WO<sub>2</sub>  
319 phase present in the 20 GPa data. Some of the peaks for *hpm*-WO<sub>2</sub> were present in the 55 GPa  
320 data, though other peaks in these data could not be indexed as *hpm*-WO<sub>2</sub> and represent a  
321 coexisting phase assumed to be another tungsten oxide. The intensity of W diffraction relative to  
322 the oxide decreased in this pressure range, suggesting that perhaps the second, non-*hpm*-WO<sub>2</sub>  
323 oxide phase was the result of the reduction of WO<sub>2</sub> and oxidation of W to form a lower valence  
324 tungsten oxide, perhaps W<sub>2</sub>O<sub>3</sub> (W<sup>3+</sup>). The intensity of WC diffraction remained nearly constant  
325 across the high pressure data. Plots of the highest temperature spectra from the 20, 40, 55 and 70  
326 GPa data are shown in Figure 4, illustrating the changes in the phase complement in the LHDAC  
327 experiments. The diffraction spectra show the change in crystal structure observed for WO<sub>2</sub> from  
328 *Pnma* to *C2/c*, the decrease in W relative peak intensities, and the appearance of WC peaks at 40  
329 GPa. The *hpm*-WO<sub>2</sub> phase was identified in both 29 GPa and 39 GPa diffraction patterns at 300  
330 K (room temperature compression), but was entirely absent in the high temperature data in the 40

331 GPa range. This places the possible phase boundary between *hp*-WO<sub>2</sub> and *hpm*-WO<sub>2</sub> over a  
332 range of ~23 to 39 GPa. Lack of high temperature data in this pressure range leads to the  
333 simplest choice for the phase boundary at approximately 32 GPa. A phase diagram for W+WO<sub>2</sub>  
334 is shown in Figure 5.

335 During EOS fitting, described in the following section, the robustness of the *hpm*-WO<sub>2</sub> phase  
336 identification in the 70 GPa data was brought into question. The misfit of the 40, 55 and 70 GPa  
337 data were not randomly distributed and showed distinct groupings above and below the zero axis  
338 and the RMSE of the fit was approximately 2 GPa. Fit quality improved when not including the  
339 70 GPa data with a reduction of the RMSE to 0.28 GPa. The additional oxide peaks in the 55  
340 GPa data not belonging to the *hpm*-WO<sub>2</sub> phase were likely from another W-oxide phase. This  
341 other phase increased in abundance in the 70 GPa data evidenced by the increase in relative  
342 abundance of these peaks and a corresponding decrease in the W peaks. These observations may  
343 signal an incomplete phase transition in which the *hpm*-WO<sub>2</sub> phase was transforming to yet  
344 another WO<sub>2</sub> structure. Assuming this was this case, the decreased number of *hpm*-WO<sub>2</sub> peaks  
345 and increased lattice parameter uncertainties at 70 GPa was the result of a mixed-phase state  
346 similar to that observed in low temperature compression where coexisting *ap*-WO<sub>2</sub> and *hp*-WO<sub>2</sub>  
347 phases resulted in poorer quality lattice parameter fits for these phases. The 70 GPa were not  
348 included in the EOS fit for *hpm*-WO<sub>2</sub>.

349 Finally, the temperatures and pressures of boundaries between the WO<sub>2</sub> phases (*P2/c*, *Pnma*,  
350 and *C2/c*) are not well constrained here (only at ~ 4 GPa and 300-500 K for *P2/c* and *Pnma*), and  
351 could be a focus of future investigations.

## 352 **Tungsten Carbide**

353 For the LHDAC experiments, tungsten carbide (WC) was present in all x-ray diffraction

354 spectra at pressures greater than 40 GPa. The source of the carbon to produce WC was likely  
 355 from the diamond anvils during laser heating, as has been observed previously in laser heated  
 356 experiments (e.g., Prakapenka et al. 2003). The diffraction peaks had low relative intensity and  
 357 remained essentially the same intensity across the high pressure data sets. Lattice parameter  
 358 values and unit-cell volumes are listed in Supplementary Data (Table S5). WC was also observed  
 359 in diffraction data in the MAP experiments. Unlike the LHDAC experiments, the small WC  
 360 peaks observed in multi-anvil runs are most likely due to C source in the assembly such as  
 361 acetone or adhesive, rather than from the WC cubes or graphite x-ray windows in the assembly.

## 362 **Results and discussion**

### 363 **Equations of state**

364 Thermal equations of state (EOS) describe the relationship between pressure, temperature,  
 365 and volume for a given phase. To calculate the WWO fO<sub>2</sub> buffer (see next section), a thermal  
 366 EOS for each of the observed WO<sub>2</sub> phases and for W was needed. The P-V-T data for each  
 367 phase were fit to Mie–Grüneisen equations of state,

$$368 \quad P = P_{298}(V) + \left(\frac{\gamma}{V}\right) [E(\theta_D, T) - E_{298}(\theta_D, T = 298)] \quad (1)$$

369 where the room-temperature pressure component,  $P_{298}$ , is represented by a 3rd order Birch-  
 370 Murnaghan EOS, and is a function of volume only;  $P_{298} = 3K_T f(1 + 2f)^{5/2} (1 + 1.5(K_T' - 4)f)$ ,  
 371 where  $K_T$  is the isothermal bulk modulus,  $K_T'$  is the bulk modulus pressure derivative, and the  
 372 Eulerian strain ( $f$ ) =  $0.5((V/V_0)^{-2/3} - 1)$  with  $V$  = volume and  $V_0$  = zero-pressure volume. A  
 373 Debye model of vibrational energy,  $E$ , was used for the thermal pressure component which  
 374 includes a Grüneisen parameter  $\gamma = \gamma_0(V/V_0)^q$  and Debye temperature  $\theta_D = \theta_0 \exp[\gamma_0/q (1 -$   
 375  $(V/V_0)^q)]$  (see Figure S1). For hp-WO<sub>2</sub>, the optimal solution is  $K_T = 230$ ,  $\gamma_0 = 1.22$  and  $q = 2.9$   
 376 with  $K_T' = 4$  fixed. Fixing  $q = 1$ ,  $K_T' = 4$ , the best fit  $K_T = 222$  and the best fit Grüneisen



377 parameter is  $\gamma_0 = 1.23$ . The difference in the r.m.s. misfits and the errors on the  $K_T$  and  $\gamma_0$   
378 parameters for these two fits are negligible. A fit with all four parameters free to vary resulted  $K_T$   
379  $= 226$ ,  $\gamma_0 = 1.43$ , and  $q = 5.2$  and  $K_T'$  unconstrained, which may reflect the relatively small  
380 pressure range of data containing this phase and an insufficient number of data to properly fit  
381 four parameters. For hpm-WO<sub>2</sub>, the optimal solution is  $K_T = 304$ ,  $\gamma_0 = 1.21$  and  $V_0 = 18.072$   
382 with  $K_T' = 4$  and  $q = 1$  fixed; a similar fit with free  $K_T'$  resulted in a larger error on  $V_0$  and with  
383  $K_T'$  approximately equal to four, and therefore  $K_T'$  was fixed at 4. A fit with all five parameters  
384 free to vary resulted identical  $K$  and  $\gamma_0$  values,  $V_0 = 18.080$ , and  $q$  and  $K_T'$  unconstrained.  
385 Because of the relatively limited temperature range of the data for ap-WO<sub>2</sub>, the overall fit was  
386 relatively insensitive to changes of the Grüneisen parameter. Setting  $\gamma_0 = 1$  or 2 resulted in an  
387 increase of approximately 0.1 GPa r.m.s. misfit with the bulk modulus,  $K_T = 238$ , unchanged.  
388 These optimal equation of state parameters are listed in Table 1 and the equation of state for  
389 WO<sub>2</sub> is plotted along isotherms in Figure 6.

390 The EOS for W was used as the pressure calibration for our data from MAP and DAC  
391 experiments ranging 300 to 2250 K, and 2 to 72 GPa. We refitted the EOS of Dorogokupets and  
392 Oganov (2007) to a Mie–Grüneisen EOS. The resulting bulk modulus and pressure derivative  
393 were 307 ( $\pm 0.40$ ) GPa and 4.05 ( $\pm 0.04$ ) GPa, respectively, which compared well with the values  
394 306 GPa and 4.17 GPa from Dorogokupets and Oganov (2007). The r.m.s. misfit of our refitted  
395 equation of state to the Dorogokupets and Oganov (2007) equation state was only 0.04 GPa over  
396 the pressure and temperature range of this study. The overall fit was optimized by inclusion of  
397 both thermal parameters. Fitting with  $q = 1$  required a change in  $\gamma_0$  of approximately 0.1 and  
398 increased the r.m.s. misfit by the same amount. Fixing  $\gamma_0 = 1.5$  and  $q = 1$  increases r.m.s. by  
399 approximately 0.1 GPa.

400 **The W-WO<sub>2</sub> oxygen fugacity buffer (WWO)**

401 With equations of state for both W and WO<sub>2</sub>, the 1-bar WWO fO<sub>2</sub> buffer (O'Neill and  
402 Pownceby 1993) was extended to high pressures, which allowed for calculating the fO<sub>2</sub> at any P  
403 or T conditions (Campbell et al. 2009). The Gibbs free energy difference on the WWO buffer is

$$404 \quad \Delta G_{WWO} = G_{WO_2} - G_W = RT \ln f(O_2) \quad (2)$$

405 Given that  $d(\Delta G) = -\Delta SdT + \Delta VdP$  and that  $dT = 0$  along an isotherm,

$$406 \quad \Delta G_{WWO(P,T)} = \int_{P=1bar}^P \Delta VdP + \Delta G_{WWO(P=1bar,T)}^* \quad (3)$$

407 which shows that the pressure dependence of the WWO buffer is related to the volume  
408 difference ( $\Delta V$ ) between W and WO<sub>2</sub>. Combining Equations 2 and 3 gives:

$$409 \quad \ln f(O_2) = \left( \ln f(O_2)_{1bar} + \int_{P=1bar}^P \Delta VdP \right) / RT \quad (4)$$

410 The WWO buffer was calculated over a pressure range of 1 bar to 70 GPa in 1 GPa  
411 increments and over a temperature range of 250 to 2500 K in 250 K increments. The 1-bar values  
412 were calculated using the equation of O'Neill and Pownceby (1993),  $fO_2|_{WWO} = -596,087 +$   
413  $300.5T - 15.97T * \ln(T)$ . Calculations above 1700 K were an extrapolation of the O'Neill and  
414 Pownceby (1993) data and were necessary for extension of the 1 bar buffer to higher pressures  
415 and temperatures. The fO<sub>2</sub> along the WWO buffer was calculated along isotherms for  $P > 1$  bar  
416 using Equation 4 to generate a matrix of fO<sub>2</sub> values. The equations of state for W and WO<sub>2</sub> were  
417 inverted to determine the required  $\Delta V$  values to solve the integral in Equation 4. Multiple WO<sub>2</sub>  
418 phases made it necessary to apply more than one equation of state. At equilibrium and along the  
419 *ap*-WO<sub>2</sub>-*hp*-WO<sub>2</sub> and *hp*-WO<sub>2</sub>-*hpm*-WO<sub>2</sub> phase boundaries, the chemical potentials of the  
420 coexisting phases are equal, and therefore the integration in Equation 4 was carried across these  
421 phase boundaries.

422 The calculations described above produced matrices of  $fO_2$  values with isothermal rows  
423 and isobaric columns. These data are adequate for plotting curves, but to facilitate rapid  
424 calculation of the  $fO_2$  of the WWO buffer at any P–T condition, the tabular (matrix) data were fit  
425 to three polynomial expressions, one each for the three  $WO_2$  phases. The polynomial form used  
426 was,  $\log fO_2|_{WWO} = (A_0 + A_1P) + (B_0 + B_1P + B_2P^2)/T$ . The temperature and pressure ranges of  
427 data used for the fits, and the  
428  $\log fO_2 = (a_0 + a_1P + a_2P^2 + a_3P^3) + (b_0 + b_1P + b_2P^2 + b_3P^3)/T$  fit parameters and the  
429 r.m.s. misfit are shown in Table 2. The WWO buffer was calculated along isobars using these  
430 expressions and these are plotted as a function of inverse temperature in Figure 7. Data points  
431 from the tabular data are plotted as points on Figure 7 to illustrate the quality of the fits. The  $fO_2$   
432 along the WWO buffer is positively correlated with temperature and pressure indicating that the  
433 system becomes more oxidizing at higher temperatures and pressures. The calculated  $\log fO_2$   
434 values have very small slope change at the phase transitions in  $WO_2$ , but these are subtle; for  
435 example the difference between the curves for the intermediate and high pressure  $WO_2$  calculated  
436 at 50 GPa and 1073 K is  $\sim 0.5 \log fO_2$  unit.

437 The difference between the WWO and IW (Campbell et al. 2009) buffers is shown in Figure  
438 8. At pressures lower than 40 GPa, the WWO buffer is at a higher  $fO_2$  than the IW buffer. The  
439 magnitude of this difference decreases at higher pressures. The significance of this relationship  
440 between the WWO and IW buffers is that it predicts the siderophile character of W. The trend of  
441 decreasing siderophile character of W shown here suggests that W will trend toward more  
442 lithophile character with increasing pressure and therefore increasing depth within the mantle. As  
443 discussed in a later section the prediction of W metal-silicate partitioning based on experimental  
444 data agrees with this conclusion.

445 Our new results can be used in high pressure experimentation to constrain oxygen fugacity  
 446 where a W capsule has been used (e.g. Cottrell et al., 2009). As one can see from our results  
 447 (Figure 8) there is little difference in IW-WWO buffer change between 1 bar and 2 GPa, so there  
 448 is no substantial correction to make to the work of Cottrell et al. (2009). However, if W capsules  
 449 are used at pressures >20 GPa, the  $fO_2$  should be calculated using our new EOS, because use of 1  
 450 bar data will result in erroneous  $fO_2$ .

451

### 452 **Application to W metal/silicate partitioning**

453 Following Campbell et al. (2009), the log of the exchange coefficient  $K_D$  for the Fe-W  
 454 exchange reaction  $2Fe + WO_2 = 2FeO + W$  as a function of the difference between the W-  
 455  $WO_2$  and IW  $fO_2$  buffers and the log of the ratio of activity coefficients is

$$456 \quad \log K_D - (\log fO_2^{WWO} - \log fO_2^{IW}) = \log \left[ (\gamma_{WO_2}^{sil} / \gamma_W^{met}) / (\gamma_{FeO}^{sil} / \gamma_{Fe}^{met})^2 \right] \quad (5)$$

457 Using the measured log  $K_D$  values from metal-silicate experiments and the calculated  
 458 differences between the WWO and IW buffers at the P-T conditions of those experiments to  
 459 calculate the left hand side, the right hand side can be rearranged as a sum of activity  
 460 coefficients, which is related to the molar excess Gibbs energy of mixing of the Fe-W exchange  
 461 reaction,

462  $G^{xs} = RT \sum_i \log(\gamma_i) = RT(\log \gamma_{WO_2}^{sil} - \log \gamma_W^{met} - 2 \log \gamma_{FeO}^{sil} + 2 \log \gamma_{Fe}^{met})$ . Oxygen fugacity  
 463 has a strong effect on W metal-silicate partitioning and this is addressed by the calculated  
 464 difference of the WWO and IW buffers, which also contains most of the non-linear pressure  
 465 dependence. We modeled the excess Gibbs energy of mixing to the first order with linear  
 466 compositional, pressure and temperature dependencies

$$467 \quad G^{xs} = RT \sum_i \log(\gamma_i) = (H^{xs} - S^{xs}T + V^{xs}P) / RT + \sum_{i,j} z_i^j X_i^j \quad (6)$$

468 where  $i$  is a component in phase  $j$  with mole fraction  $X$ , and  $H^{xs}$ ,  $S^{xs}$  and  $V^{xs}$  are the excess  
 469 enthalpy, entropy and volume of mixing, respectively. The pressure dependence in the W, WO<sub>2</sub>,  
 470 Fe and FeO activity coefficients is contained in the excess molar volume of mixing term,  $V^{xs}$ .

471 Tungsten metal-silicate partitioning cast in terms of an Fe-W exchange partition  
 472 coefficient is:

$$473 \quad \log K_D = [\log fO_2^{W^{WO}} - \log fO_2^{IW}] + [(H^{xs} - S^{xs}T + V^{xs}P)/RT + \sum_{i,j} z_i^j X_i^j] \quad (7)$$

474 The excess Gibbs energy of mixing was fitted for molar metal–silicate exchange partition  
 475 coefficients that were calculated from literature data (Walter and Thibault, 1995; Hillgren et al.,  
 476 1996; Ohtani et al., 1997; Righter and Shearer, 2003; Cottrell et al., 2009; Wade et al., 2012) and  
 477 from unpublished data of Shofner et al. These partition coefficients were obtained from the  
 478 measured mole fraction abundances of Fe and W in both the metallic and silicate phases. The  
 479 phase components modeled as contributing to  $G^{xs}$  were SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and CaO in the silicate melt,  
 480 and S in the metallic melt, and the results of this fit are shown in Table 3. It was assumed that the  
 481 activity coefficients were the same for all WO<sub>2</sub> phases; this may be unlikely, but in the absence  
 482 of any information otherwise we make this provisional assumption for these calculations.

483 The metal/silicate partitioning of W using Equation 7 was calculated along the peridotite  
 484 liquidus, shown as curve B in Figure 9, and along isobars (Figure 10). A regression based on  
 485 linear dependencies in all parameters is shown for comparison in Figures 9 and 10; the  
 486 regression equation

$$487 \quad \log K_D = 2.00 - (3180 / T) - (125 P / T) + (0.52 X_C) - (4.27 X_S) \quad (8)$$

488 was fitted to the data and calculated along the peridotite liquidus, where  $X_C$  and  $X_S$  are the mole  
 489 fractions of carbon and sulfur, respectively, in the metallic Fe. Partitioning along the liquidus  
 490 curves using Equations 7 and 8 have generally the same trend, with Equation 7 predicting a

491 larger decrease in the siderophilicity of W with increasing pressure. The slope change in curve B  
492 at ~ 33 GPa is due to the difference in  $fO_2$  calculated for the higher pressure form of  $WO_2$ .  
493 Early work on W partitioning revealed non-ideality in both the metallic and silicate liquids (e.g.,  
494 S and C content of metal (Jana and Walker, 1997a,b) and degree of polymerization in silicate  
495 melt (Walter and Thibault, 1995)), making isolation of pressure effects difficult and perhaps  
496 even unlikely. The agreement between our results on the pressure effects for the metal-oxide end  
497 member and multi-component systems is perhaps unexpected and therefore worth highlighting  
498 here.

499         Pressure and temperature have competing effects on the metal/silicate partitioning of W.  
500 In the previous paragraph we have demonstrated that  $\log K_D$  decreases at higher pressures. Yet,  
501 calculated along isobars by Equation 7,  $\log K_D$  is positively correlated with temperature where  
502 the temperature effect is approximately 0.5 log units at 20 GPa, increasing to approximately 2.5  
503 log units at 60 GPa between 2000 and 3000 K (Figure 10). However, in the more naturally  
504 realistic case, along the peridotite liquidus where both pressure and temperature vary, pressure  
505 exerts the greater effect. A comparison of Equation 7 to other predictive expressions of  $K_D^{W(met-  
506 sil)}$  (Siebert et al. 2011; Wade et al. 2012) is shown in Figure 11. The prediction of Equation 7  
507 (curve B) is similar to that of Siebert et al. (2011) (curve A) at lower pressures but the curves  
508 diverge at higher pressures where the separation of the curves increases to 0.7 log units at 60  
509 GPa. Wade et al. (2012) concluded that W metal-silicate partitioning has no significant pressure  
510 dependence and this is shown by the essentially flat trend of curve C in Figure 11 across the  
511 pressure range of 0 – 60 GPa. This is contrary to the findings of the present study and that of  
512 Siebert et al. (2011). Using a predictive expression for  $\log D_W$  from Cottrell et al. (2009, 2010)  
513 and calculating W metal-silicate partitioning along the peridotite liquidus indicates an increase in

514 the lithophile behavior of W at higher pressures. While the Cottrell et al. (2009, 2010) expression  
515 was not in terms of the Fe-W exchange coefficient, it results in the same trend of decreasing W  
516 siderophile behavior at higher pressures.

517 The difference in the prediction of W metal-silicate partitioning by Equation 7 and  
518 Siebert et al. (2011) is likely due to different approaches to modeling the pressure dependence of  
519  $fO_2$ , which has a strong influence on W metal-silicate partitioning. This is better characterized by  
520 the measure of the volume difference between WWO and IW buffers as opposed to the simple  
521 linear approximation of  $\Delta IW$ . The pressure effect on  $fO_2$  is captured by the equations of state  
522 underlying the buffers that more precisely represent the volume changes at higher pressures  
523 where non-linearity is more pronounced. The pressure dependence of W metal-silicate  
524 partitioning is relatively small and therefore the difference between the linear and non-linear  
525 (buffer-based) approaches is correspondingly small. However, it is likely that this difference  
526 would be higher for other elements, e.g. Ni which has strong pressure dependence (Campbell et  
527 al. 2009). Additional partitioning experiments at pressures higher than 30 GPa should also  
528 improve the agreement between the two approaches (e.g., Shofner et al., 2014), since the  
529 partitioning data is currently limited to pressures < 25 GPa.

530

### **Implications**

531 Tungsten is a geochemically important element that has bearing on both the process and timing  
532 of core formation in the Earth. The effect of the redox state of W on its geochemical behavior at  
533 conditions of the deep Earth are crucial for accurate and precise determination of W properties  
534 and behavior in core formation and other geochemical modeling. Extension of the 1-bar WWO  
535 buffer to high pressures can improve its application in both deep Earth and high pressure  
536 experimental applications. High pressure experimentation in this study identified a previously

537 unknown high-pressure phase of  $\text{WO}_2$  that contributes to better understanding of the WWO  
538 buffer at high pressure. Applying the WWO buffer to metal-silicate systems can provide  
539 improved determination of the non-linear pressure effect on W metal-silicate partitioning, and of  
540 the activity of W in both silicate and metallic phases. The ultimate contribution of this work on  
541 the WWO buffer will be to improve constraints on Earth core formation models and to allow for  
542 the use of the WWO buffer in high pressure experiments by allowing more precise calculation of  
543  $f\text{O}_2$ .

544

545

### **Acknowledgements**

546 This research was supported by a NASA GSRP fellowship to GAS, NASA RTOP from the  
547 Cosmochemistry program to KR, and NSF grant EAR-1243847 to AJC. RAF was supported by  
548 the NSF GSFP and a Flagship Fellowship from University of Maryland. High pressure multi-  
549 anvil assemblies were produced by the COMPRES Infrastructure Development Project. Portions  
550 of this work were performed at GeoSoilEnviroCARS (Sector 13), Advanced Photon Source  
551 (APS), Argonne National Laboratory. GeoSoilEnviroCARS is supported by the National Science  
552 Foundation - Earth Sciences (EAR-1128799) and Department of Energy- GeoSciences (DE-  
553 FG02-94ER14466). This research used resources of the Advanced Photon Source, a U.S.  
554 Department of Energy (DOE) Office of Science User Facility operated for the DOE Office of  
555 Science by Argonne National Laboratory under Contract No. DE-AC02-06CH11357. Assistance  
556 with RHDAC experiments was provided by undergraduate researcher James Deane. Reviews by  
557 D. Walker, C. Lesher, and several anonymous reviewers helped improve the clarity of the  
558 manuscript.



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### Figure Captions

661 **Figure 1.** Pressure and temperature distributions of x-ray diffraction experiments. MAP – multi-  
662 anvil press, LHDAC – laser-heated diamond anvil cell, RHDAC – resistively-heated diamond  
663 anvil cell, and DAC 300K – room-temperature compression in diamond anvil cell. The data  
664 points are only those used in the EOS fit. There were higher pressure/temperature data collected,  
665 but the limited number of peaks and the uncertainties on the volumes made the data unsuitable  
666 for inclusion in the EOS.

667 **Figure 2.** X-ray diffraction spectrum showing patterns G33\_006 and G33\_022. The *hp*-WO<sub>2</sub>  
668 (*Pnma*) phase of WO<sub>2</sub> described by Sundberg et al. (1994) is present in spectrum 006 but is not  
669 present in 022. The *d*-spacing offset between these two spectra is due to compression.

670 **Figure 3.** X-ray diffraction spectrum showing G33\_006 and a calculated pattern for the *Pnma*  
671 structure of the *hp*-WO<sub>2</sub> phase of WO<sub>2</sub> described by Sundberg et al. (1994). Peaks in high

672 pressure pattern offset in  $d$ -spacing by approximately  $-0.1 \text{ \AA}$  relative to 1-bar pattern due to  
673 compression.

674 **Figure 4.** X-ray diffraction spectra from highest temperature pattern at each pressure range. The  
675  $d$ -spacing offset between the spectra is due to compression. The 110 and 211 peaks for W are  
676 labeled to show the change in relative intensity of W to the other phases in the two highest  
677 pressure data sets.

678 **Figure 5.** Phase diagram for  $\text{WO}_2$ . Space group of phases are indicated in italics. The green  
679 symbol indicates the pressure and temperature synthesis conditions of the high pressure  
680 orthorhombic phase (*Pnma*) described by Sundberg et al. (1994). Note that the overlap of data  
681 near the  $P2_1/c$ -*Pnma* phase boundary is related to the low temperature phase dynamics as  
682 discussed in the text. The various phases and space groups of  $\text{WO}_2$  are: ap- $\text{WO}_2 = P2_1/c$ ; hp-  
683  $\text{WO}_2 = Pnma$ ; hpm-  $\text{WO}_2 = C2/c$ . Color scheme is the same as in Figure 1.

684 **Figure 6.** PVT EOS for  $\text{WO}_2$  plotted along isotherms as a function of pressure. Each phase is  
685 plotted for the pressure ranges as shown in Figure 5. The various phases and space groups of  
686  $\text{WO}_2$  are: ap- $\text{WO}_2 = P2_1/c$ ; hp- $\text{WO}_2 = Pnma$ ; hpm-  $\text{WO}_2 = C2/c$ .

687 **Figure 7.** Isobaric plot of the absolute  $f\text{O}_2$  ( $\log_{10}$ ) of the WWO buffer plotted as a function of  
688 inverse temperature. Curves were calculated using the polynomial expressions in Table 2, and  
689 the points are the fitted data from the tabulated values resulting from the extension of the 1-bar  
690 WWO buffer to high pressure.

691 **Figure 8.** Difference between WWO and IW buffers plotted as isobars as a function of inverse  
692 temperature. WWO was calculated using the polynomial expressions in Table 2, and IW was  
693 calculated using the Fe-FeO buffer of Campbell et al. (2009).

694 **Figure 9.** The predicted W metal/silicate partitioning in terms of the  $\log_{10}$  of the Fe-W exchange

695 coefficient calculated along a peridotite liquidus (Herzberg and Zhang 1996; Zerr et al. 1998).  
696 The red curve (B) was calculated using Equation 7, and for comparison, the blue curve (A) was  
697 calculated using Equation 8. The slope change in curve B at ~ 33 GPa is due to the difference in  
698  $fO_2$  calculated for the higher pressure form of  $WO_2$ .

699 **Figure 10.** Isobaric plots of the predicted W metal/silicate partitioning in terms of the log of the  
700 Fe-W exchange coefficient. Solid lines were calculated using Equation 7, and dotted lines were  
701 calculated using Equation 8.

702 **Figure 11.** Comparison of  $\log K_D^W$  calculated along the peridotite liquidus as predicted by  
703 Siebert et al. (2011) (Curve A), Equation 7 (curve B), and Wade et al. (2012) (Curve C). The  
704 liquidus is a fit to data from Herzberg and Zhang (1996) and Zerr et al. (1998).

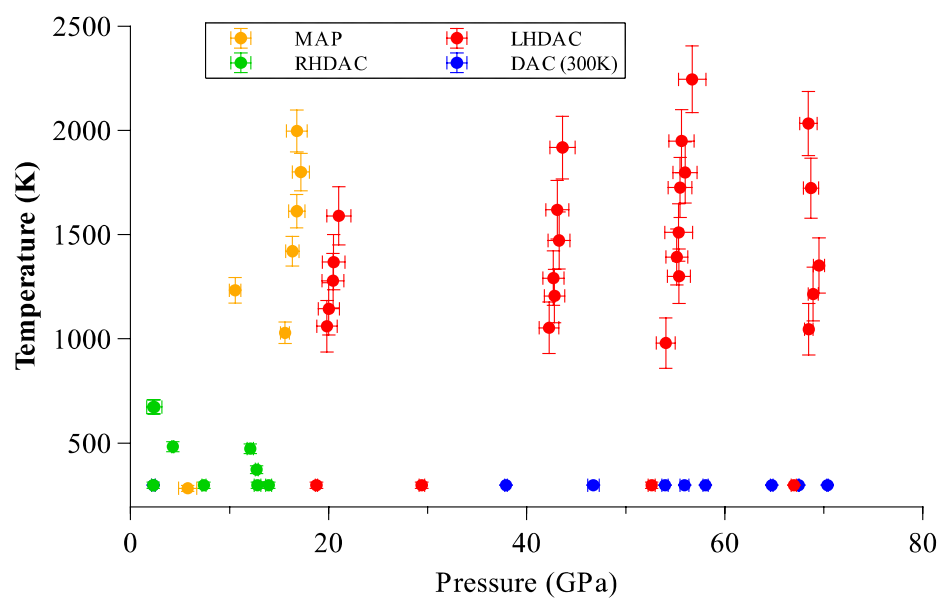


Figure 1



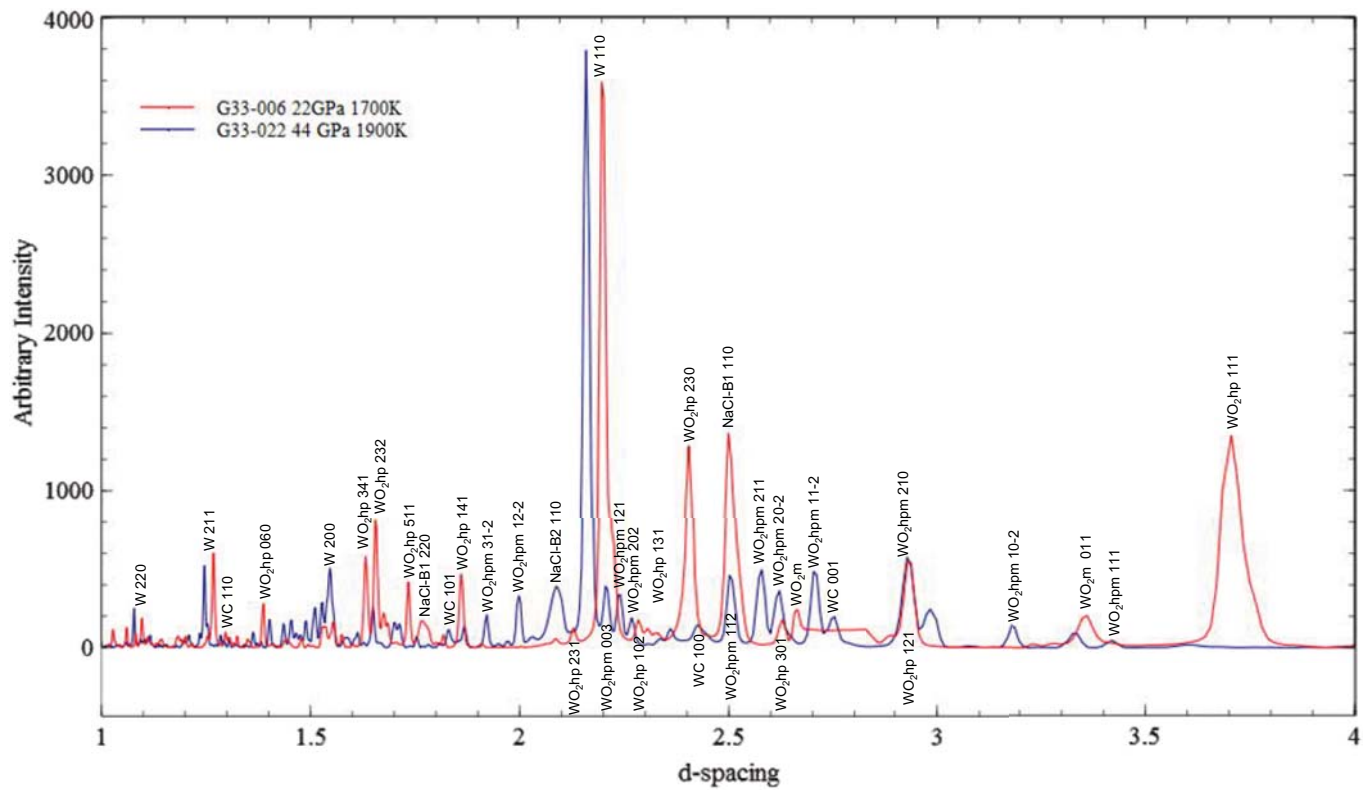


Figure 2

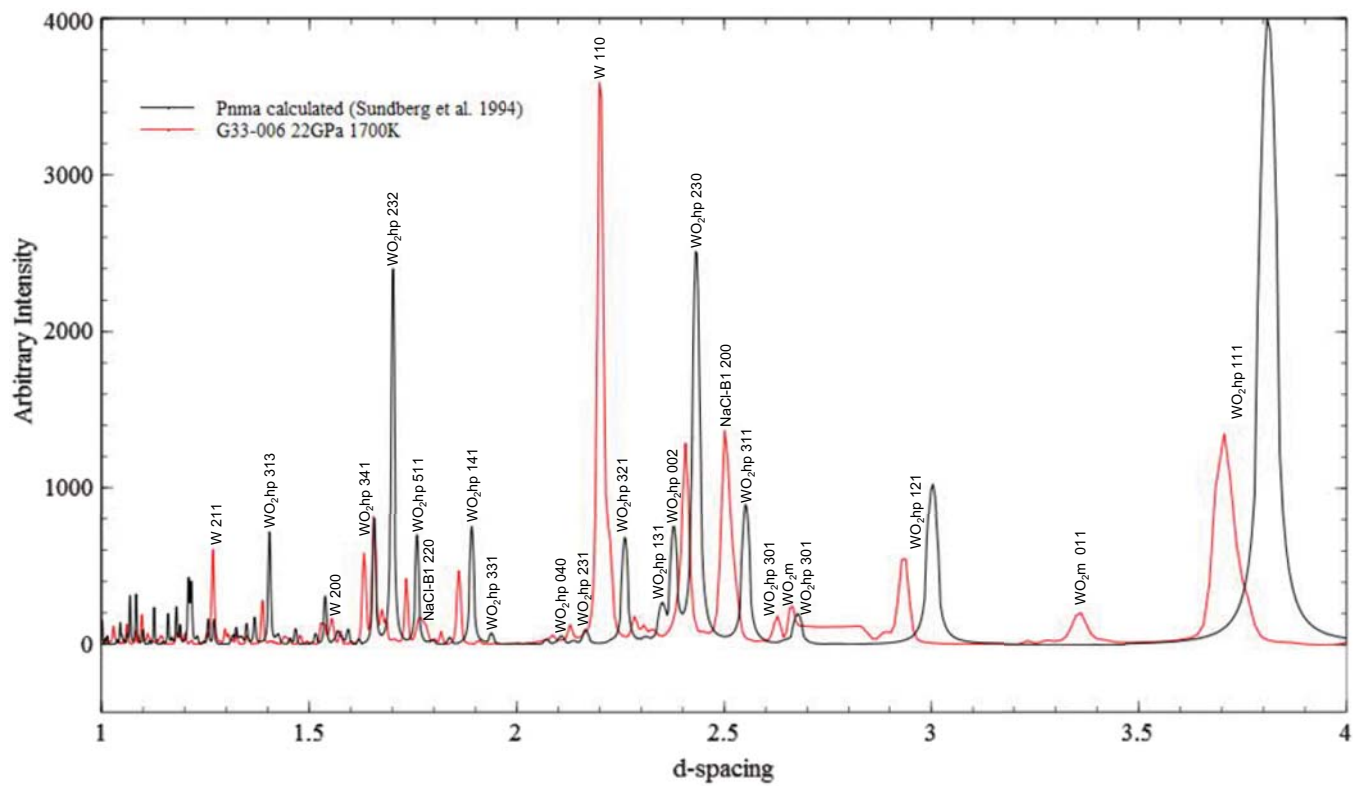


Figure 3

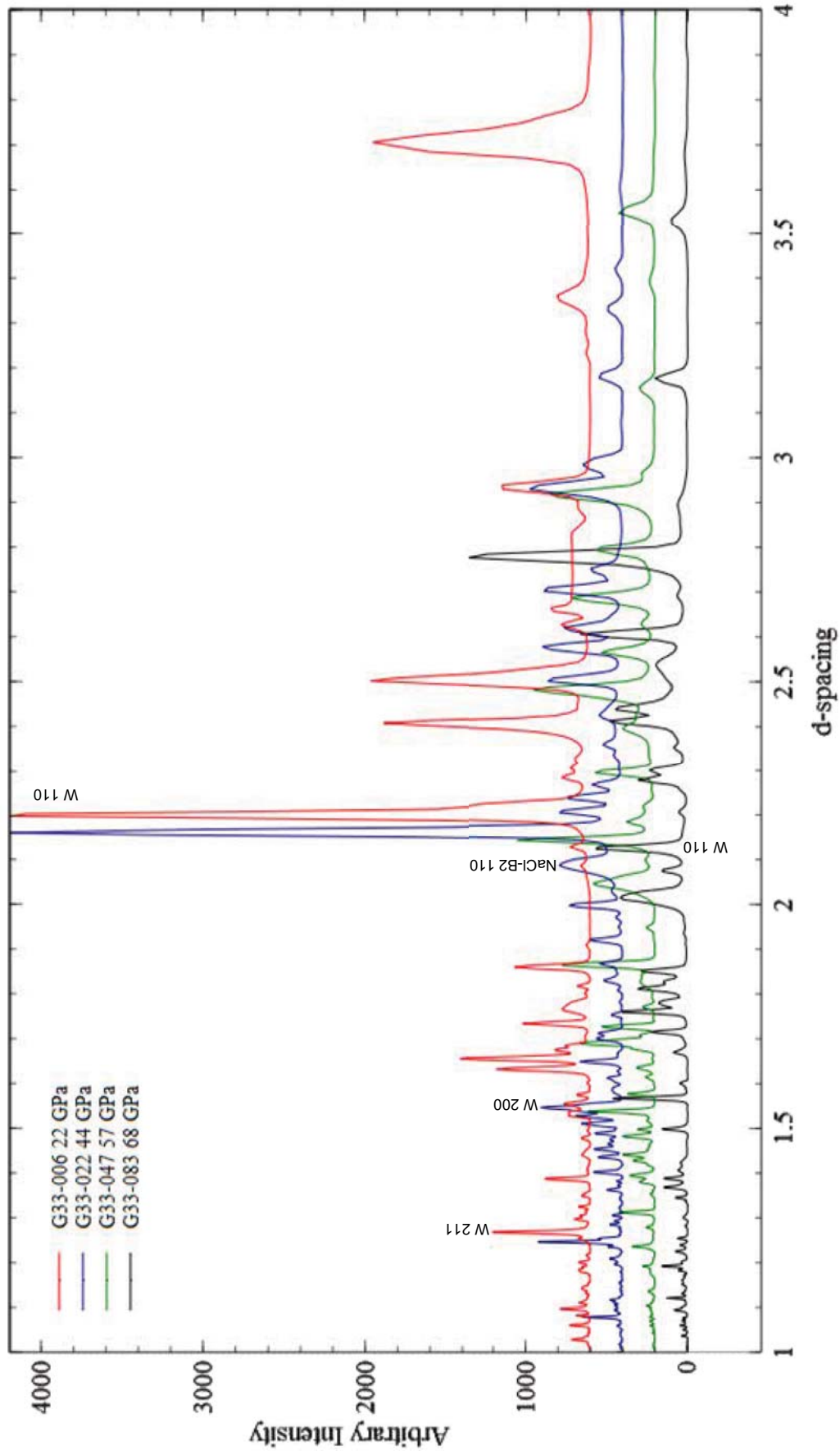


Figure 4

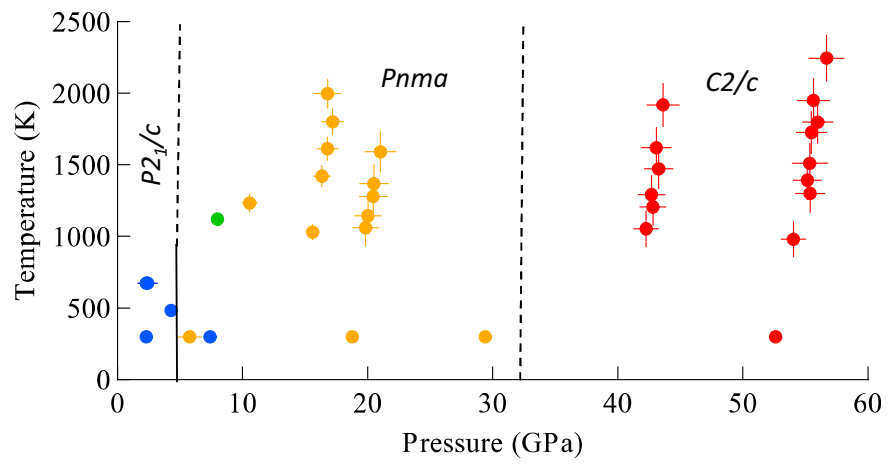


Figure 5

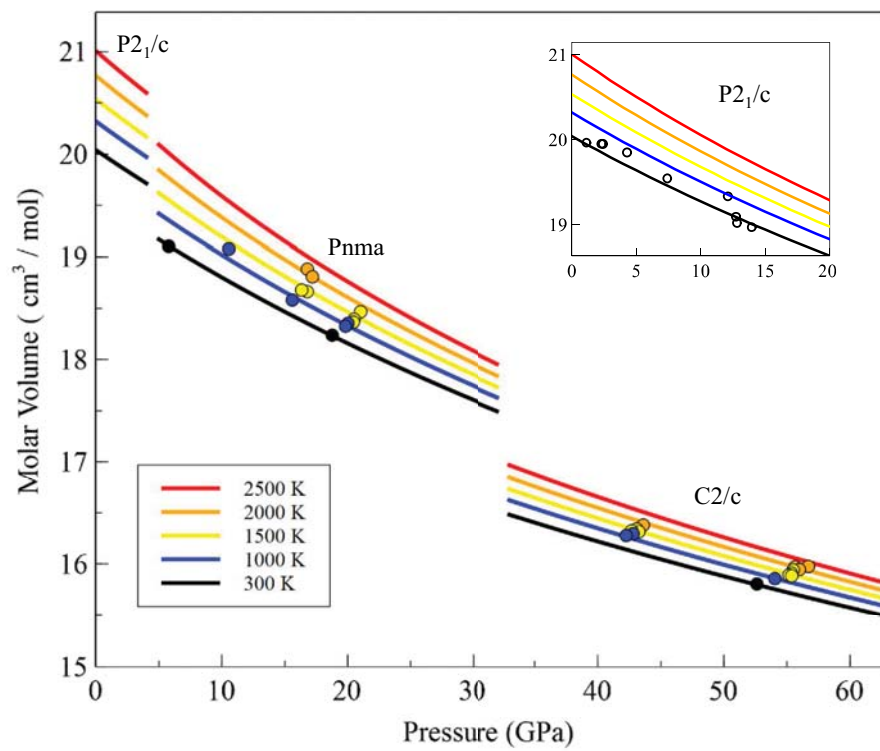


Figure 6

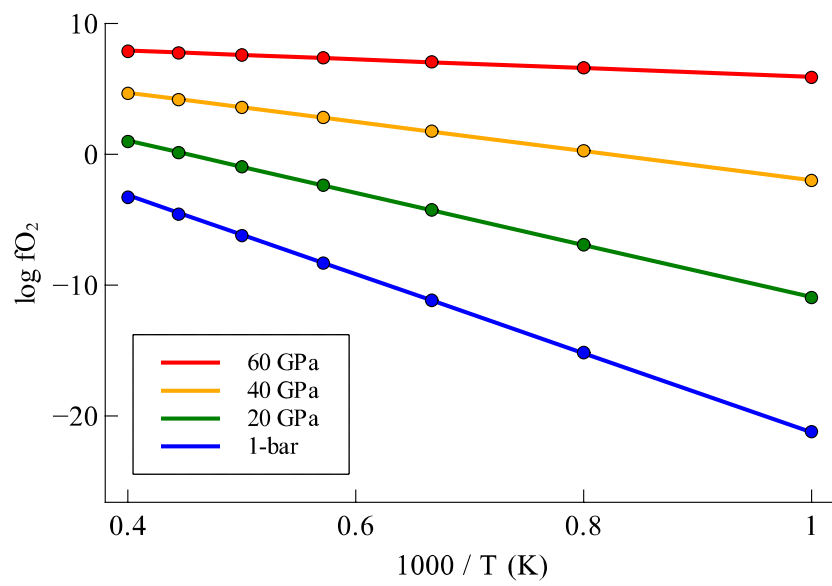


Figure 7

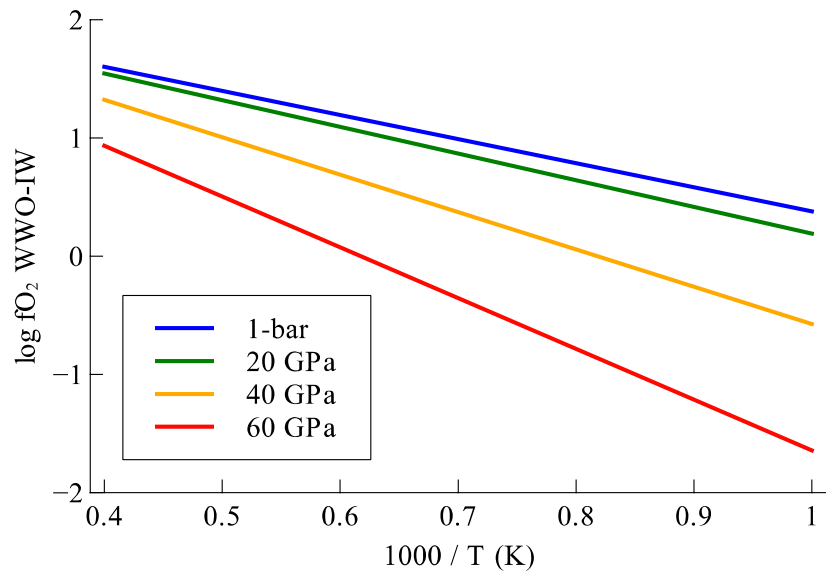


Figure 8

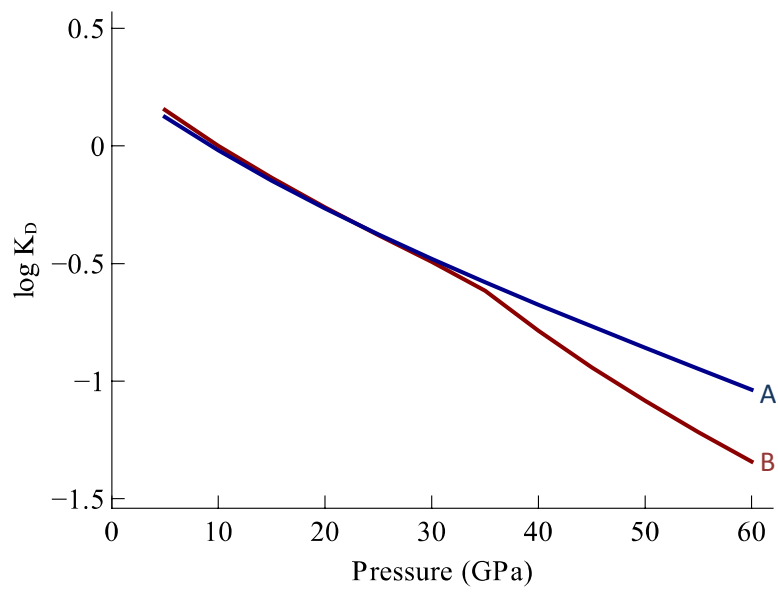


Figure 9



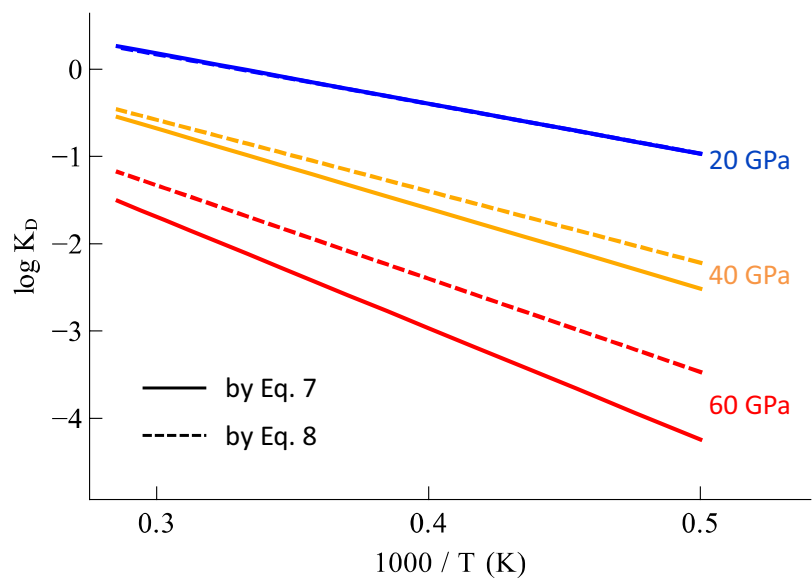


Figure 10

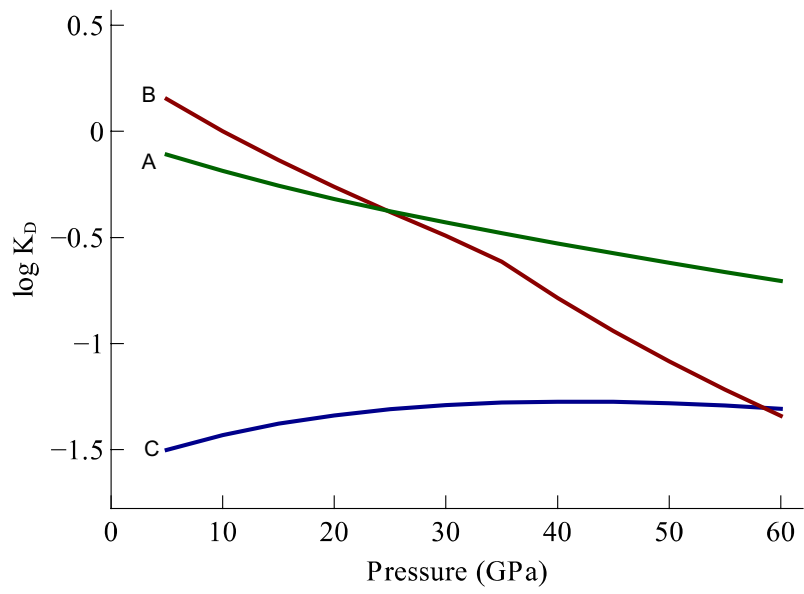


Figure 11

Table 1. Equation of state parameters (Birch-Murnaghan with Grüneisen parameter and Debye temperature).

<sup>a</sup>JCPDS card files. <sup>b</sup>Sundberg et al. (1994). <sup>c</sup>Kittel (1996). <sup>d</sup>Goodenough et al. (1984)

	W	ap-WO <sub>2</sub>	hp-WO <sub>2</sub>	hpm-WO <sub>2</sub>
V <sub>0</sub> (cm <sup>3</sup> /mol)	9.544 <sup>a</sup>	20.037 <sup>a</sup>	19.570 <sup>b</sup>	18.072 ± 0.02
K <sub>T</sub> (GPa)	307 ± 0.40	238 ± 4	230 ± 3	304 ± 3
K <sub>T</sub> ' (GPa)	4.05 ± 0.04	4 (fixed)	4 (fixed)	4 (fixed)
θ <sub>D</sub> (K)	400 <sup>c</sup>	380 ± 15 <sup>d</sup>	380 ± 15 <sup>d</sup>	380 ± 15 <sup>d</sup>
γ <sub>0</sub>	1.61 ± 0.03	1.45 ± 0.18	1.22 ± 0.07	1.21 ± 0.12
q	1.54 ± 0.13	1 (fixed)	2.90 ± 1.5	1 (fixed)
r.m.s. (GPa)	0.04	0.38	0.22	0.14

Table 2. Parameters of polynomial fits of tabulated  $fO_2$  values for  $P2_1/c$ ,  $Pnma$ , and  $C2/c$   $WO_2$  phases in the high pressure W- $WO_2$  buffer.

$$\log fO_2 |_{WVO} = (A_0 + A_1P) + (B_0 + B_1P + B_2P^2)/T.$$

$WO_2$ phase	Parameters	r.m.s.	P range (GPa)	T range (K)
ap- $WO_2$ ( $P2_1/c$ )	$A_0$ 8.957 $B_0$ -30200	0.023	0 - 4	750 - 2000
	$A_1$ 0 $B_1$ 554.2			
	$B_2$ 0			
hp- $WO_2$ ( $Pnma$ )	$A_0$ 8.860 $B_0$ -29947	0.018	5 - 32	1000 - 2250
	$A_1$ 0.007804 $B_1$ 524.1			
	$B_2$ -1.178			
hpm- $WO_2$ ( $C2/c$ )	$A_0$ 9.000 $B_0$ -27954	0.027	33 - 70	1000 - 2250
	$A_1$ 0.004493 $B_1$ 438.8			
	$B_2$ -0.479			

Table 3. Fit parameter for the excess Gibbs energy of mixing in the W-WO2 buffer-based expression of the Fe-W exchange coefficient.

$H^{XS}$	$-8.98 \pm 7.8$
$S^{XS}$	$0.0236 \pm 0.0036$
$V^{XS}$	$-1.02 \pm 0.14$
$zSiO_2$	$6.58 \pm 0.56$
$zAl_2O_3$	$7.02 \pm 1.3$
$zCaO$	$-8.27 \pm 1.0$
$zS$	$-4.49 \pm 0.72$
r.m.s.e.	0.26